



Shield block development of ITER Module 18

PFC eMeeting

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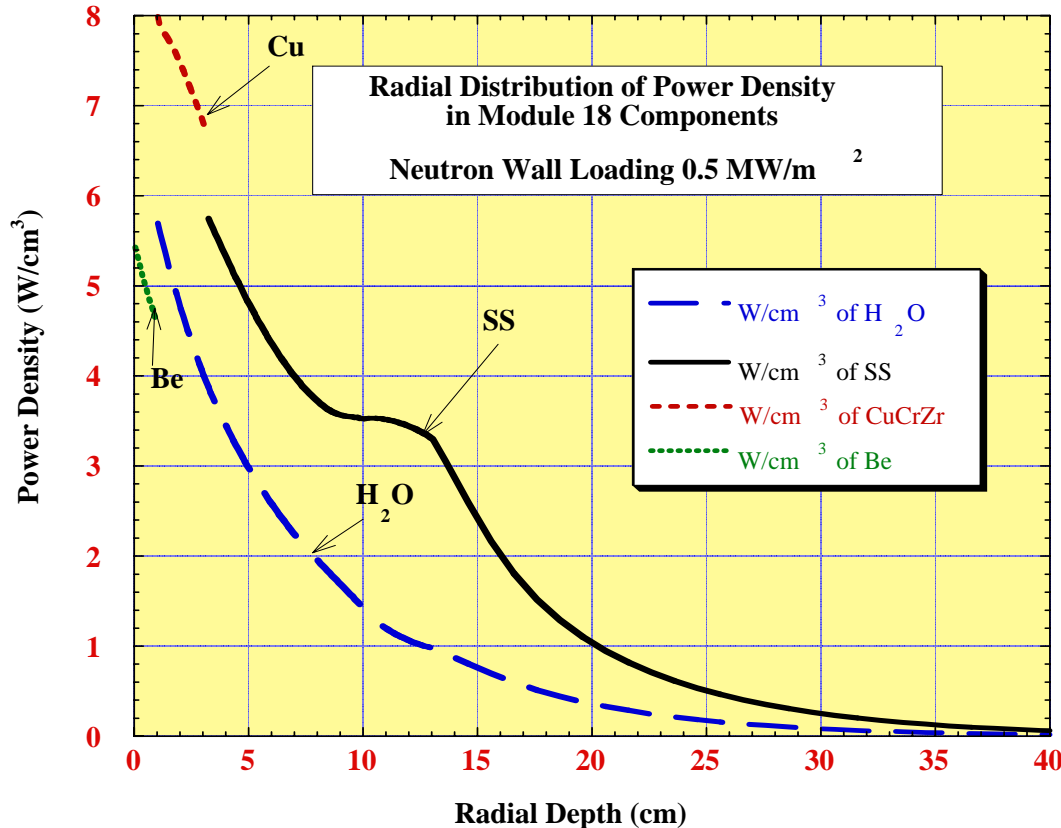
Sandia National Laboratories



Issues with IT Shield Design

- **Minimum required heat transfer coefficient for “front header” with a top plate of 20mm would be about 2000 W/m²K (using Sawan’s calculation)**
- **Chinese report calculation of heat transfer coefficient with no flow guide~1400 W/m²K, and with flow guide 4270 W/m²K**
- **But there were corners of the front reservoir which may not have enough flow velocity**
- **Dong Won Lee (KAERI) also shows that a different design is needed and has proposed a T shape that also improves flow velocity**

M. Sawan 1D nuclear heating data



Flat area of SS power density curve corresponds to 20 mm thick cover plate of the IT baseline design.

The power density here was assumed for the front side of the upside-down reservoir idea.

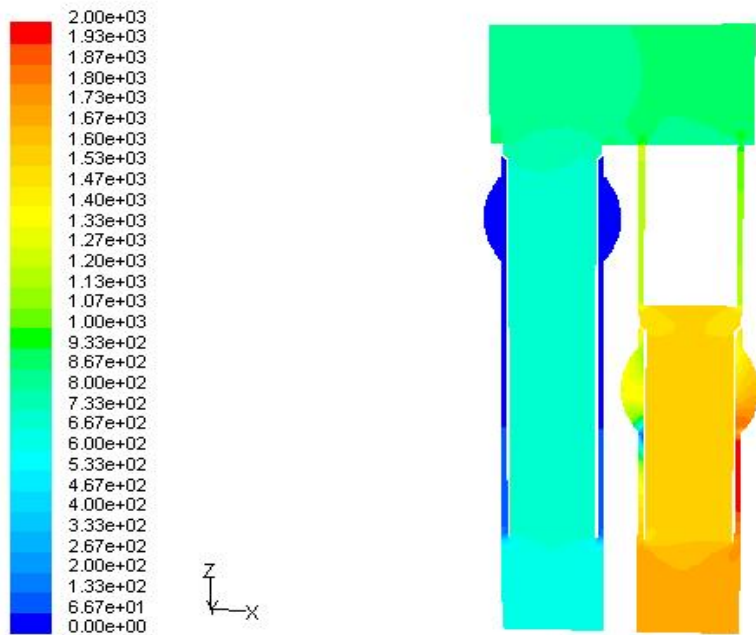
In this 1D calculation the heating distribution is calculated with a SS-water mix in the majority of the module



IT design on Module 18

- Our radial holes are 30 mm dia as this module is narrower than modules 2-6
- 20 radial holes distributed vertically
- Flow out of each hole into front reservoir is 0.044kg/s (1.76kg/s / 40 holes)
- Average heat transfer coefficient is 5500W/m²K for the front surface, but it varies a lot depending on position

Fluent & CFXDesign (IT design)

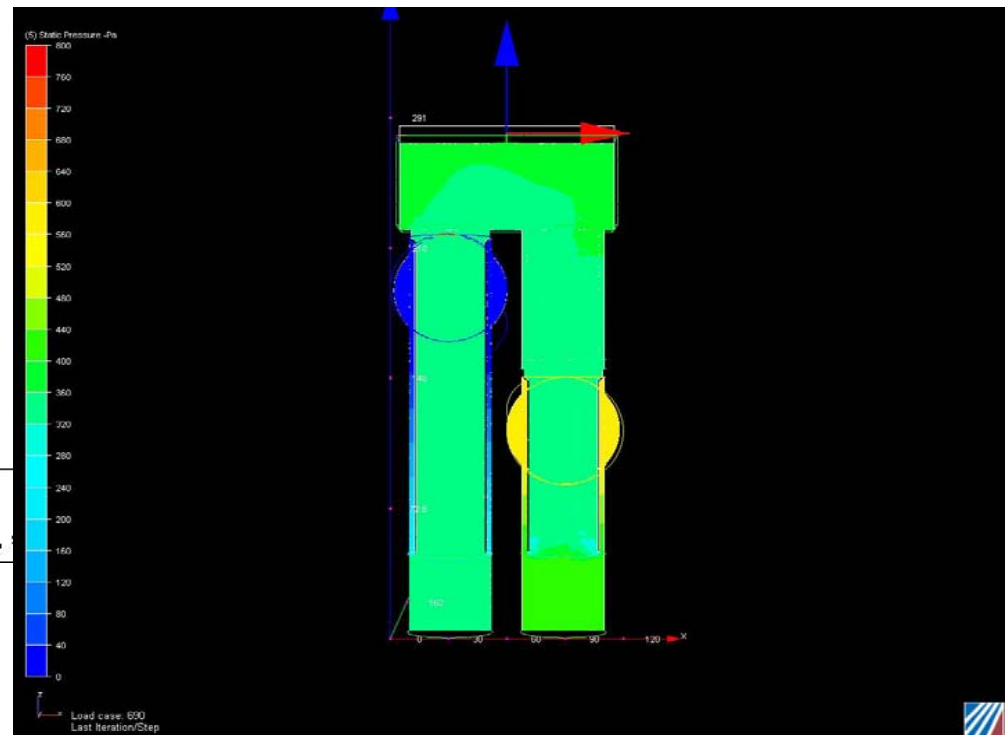


Contours of Static Pressure (pascal) (Time=7.0000e-02)

FLUENT 6.1 (3d, segregated)

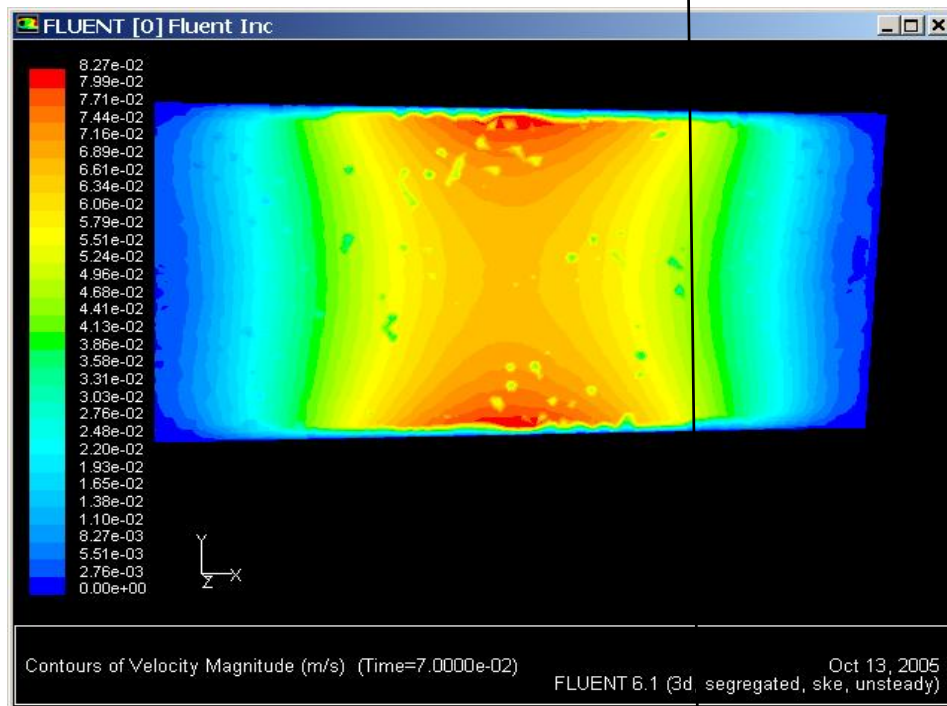
45mm dia radial holes,
2.5 mm insert clearance,
60 mm dia headers

This calculation was difficult in the region of small clearance and may need refinement.

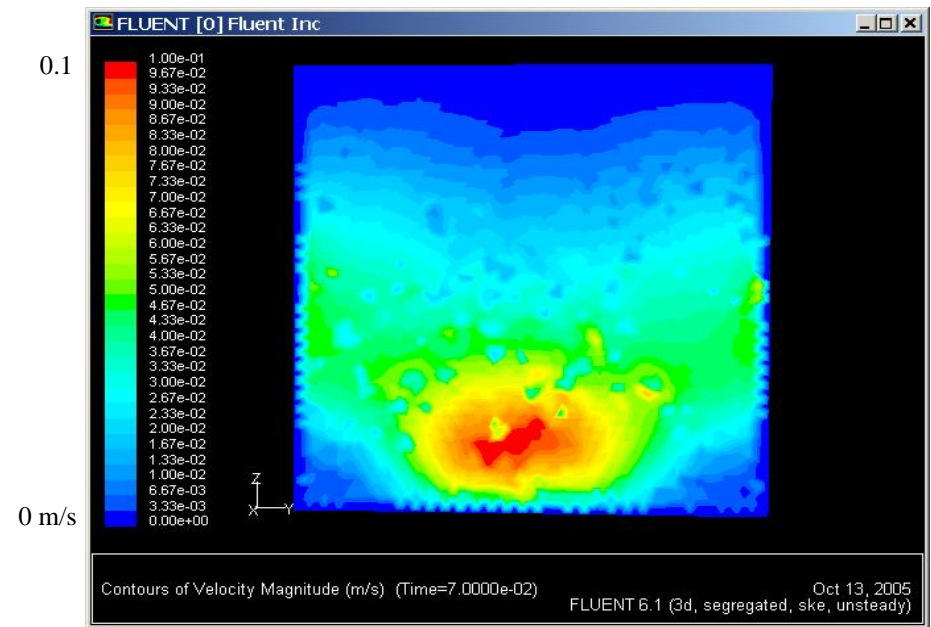


Flow velocity for Original IT design on top surface for module 18

Top surface view



Short-side view



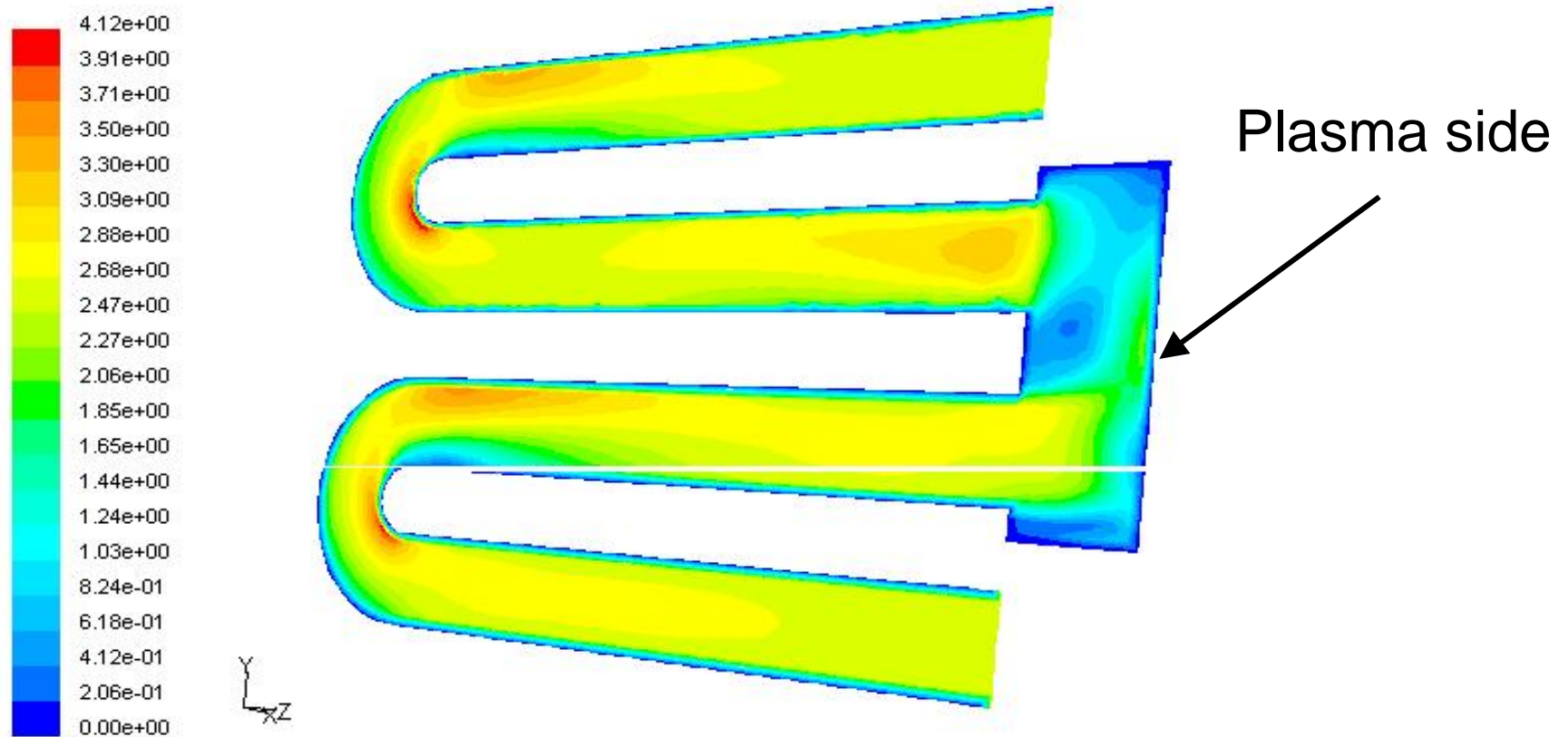
Without a driver, the flow through the top reservoir is about .06 m/s
In the outer corners, the flow is not high enough



Hydraulic analysis

- **Three computer codes are compared**
 - **Fluent**
 - **Powerful and popular code**
 - **Finite volume**
 - **Geometry import/translation required**
 - **CFDesign**
 - **Finite element**
 - **Direct CATIA input**
 - **CFD2000**
 - **Finite volume**
 - **Takes longer than CFDesign**
 - **No geometry imports**

Our original design with reservoir in the back had problems of slow velocity in the hottest region

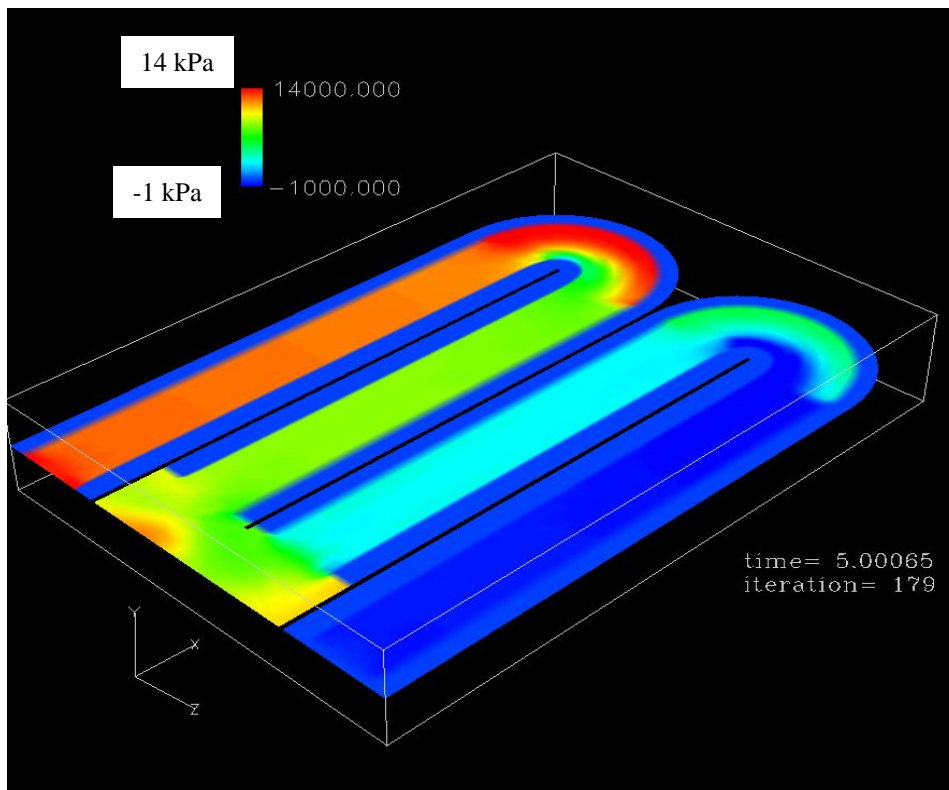


Contours of Velocity Magnitude (m/s) (Time=5.0000e-02)

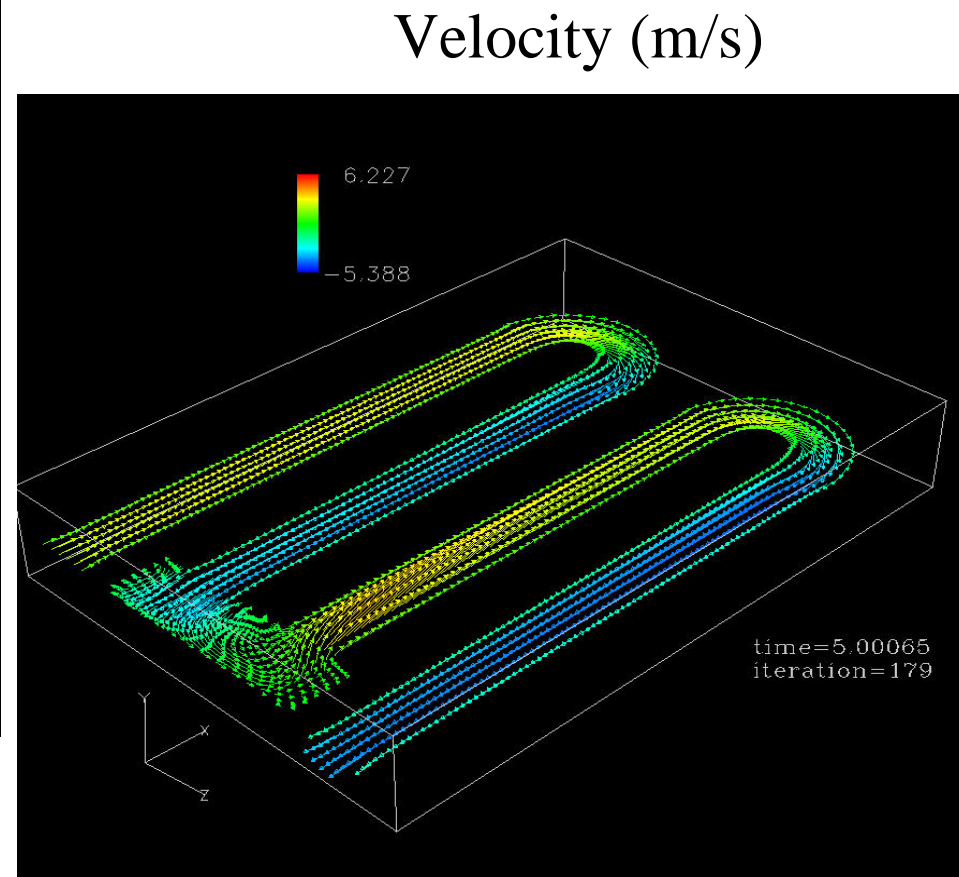
Aug 17, 2005
FLUENT 6.1 (3d, segregated, ske, unsteady)

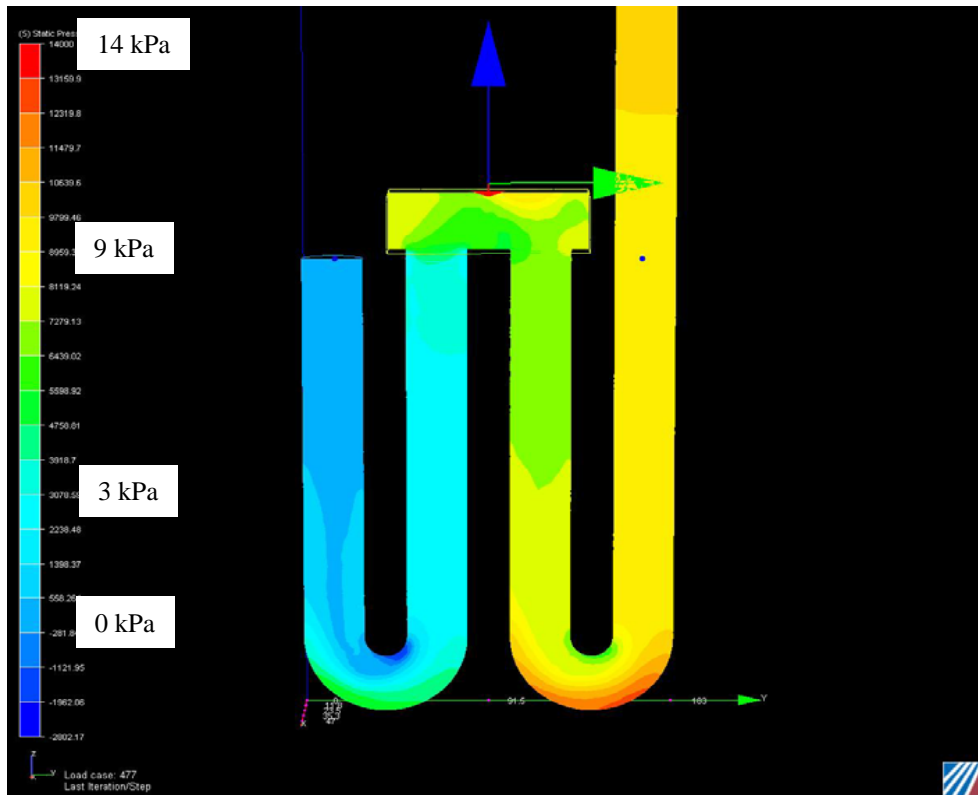
This shows the analysis of the velocity using Fluent

CFD-2000 Results US design

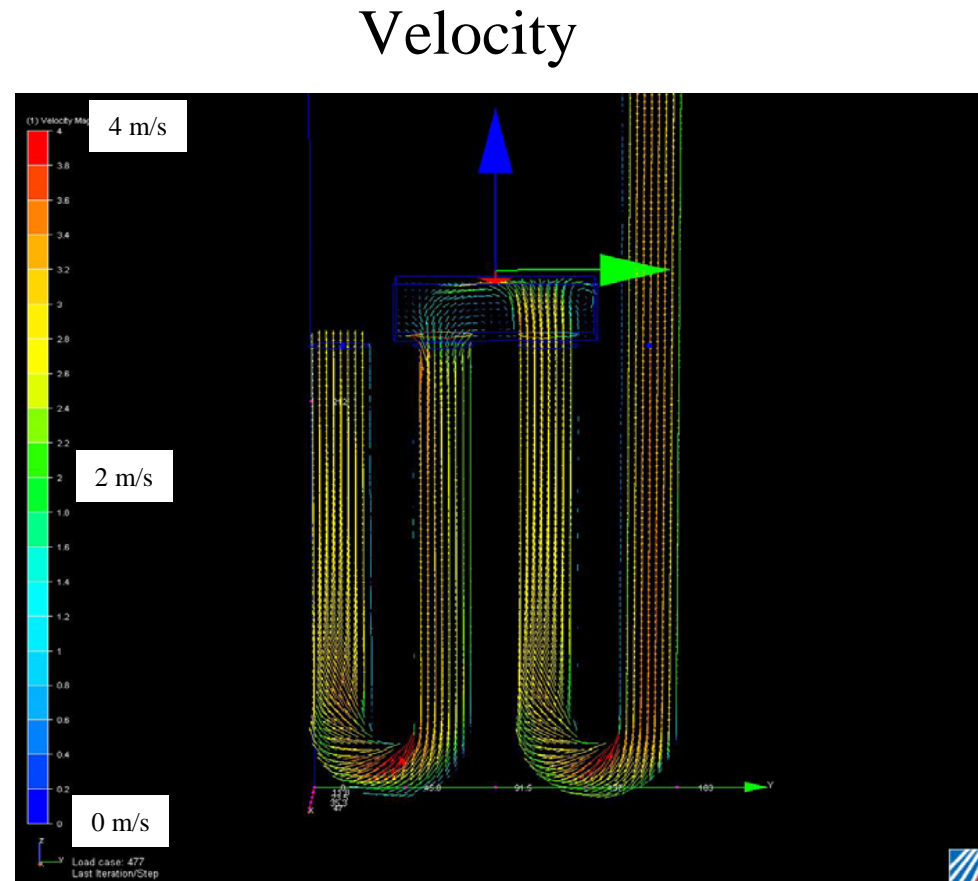


Static pressure





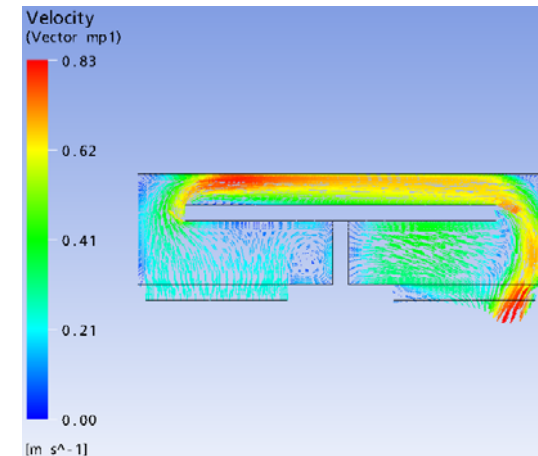
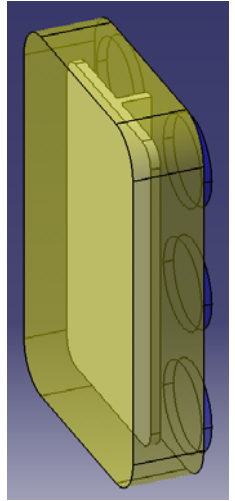
Static pressure



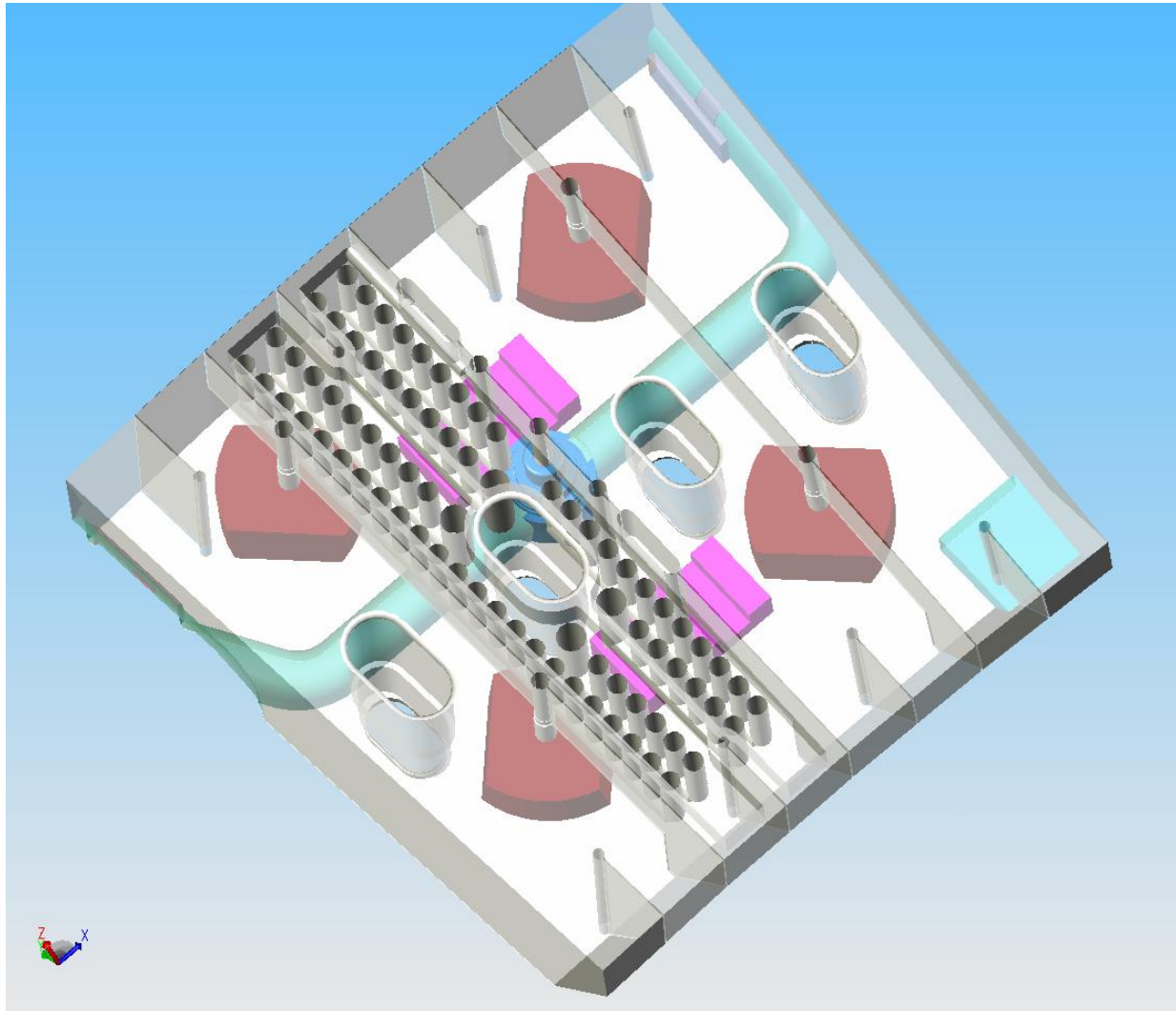
Velocity

New Idea for flow

- Explore use of Tee divertor vane in shield block reservoir as proposed by Koreans
- Change loop depth so that most material on plasma face is within 10 mm of cooling loop
- Loops are mostly in series, but break out in a few parallel paths
- 23 radial holes, 30-mm DIA
- No flow annuli in the loops – use orifice plate
- Smallest hydraulic distance is 15 mm

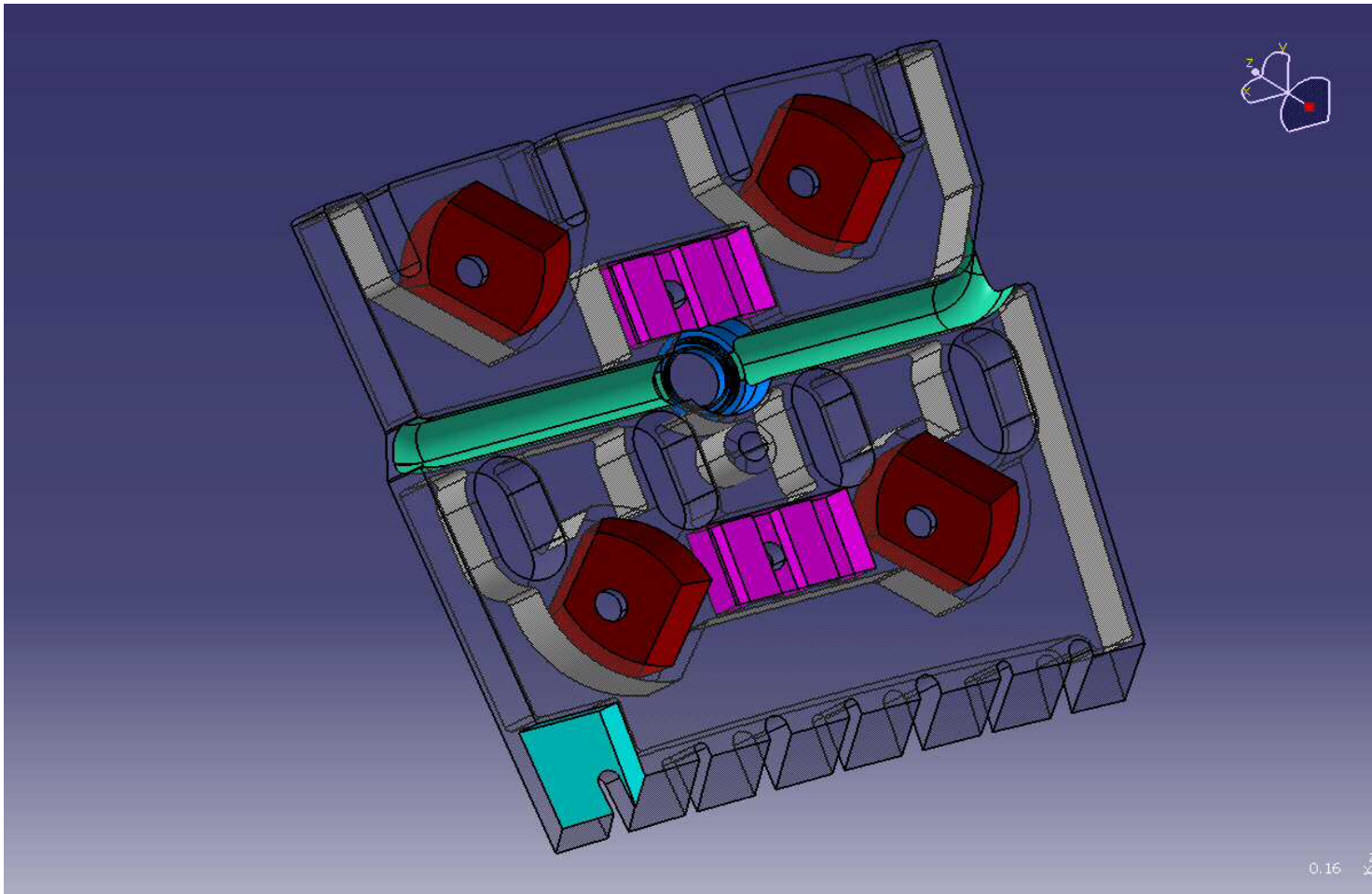


How the top surface will look

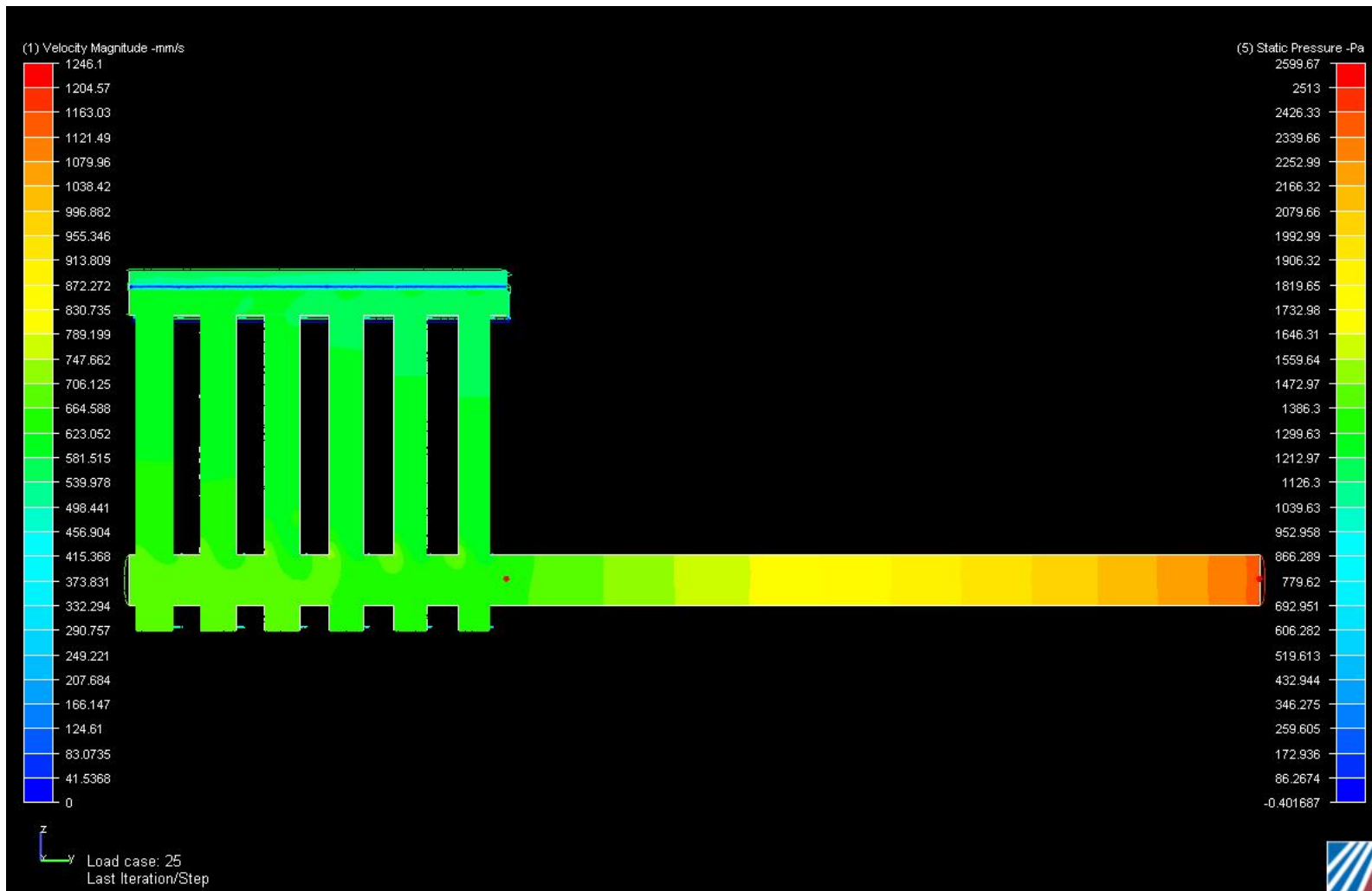




Back piece



Orificing required to obtain more uniform flow distribution.

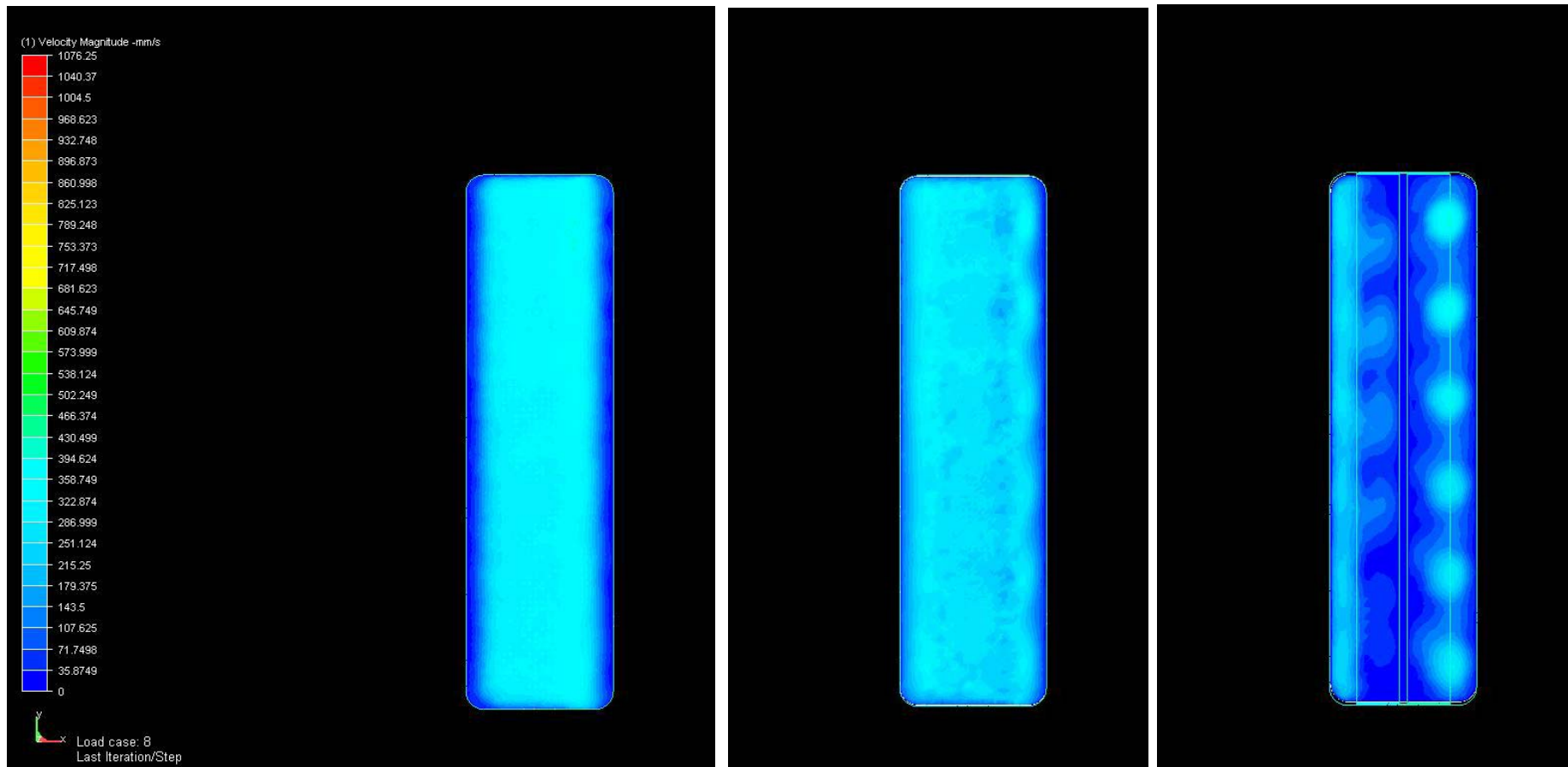


Velocity distributions in reservoir

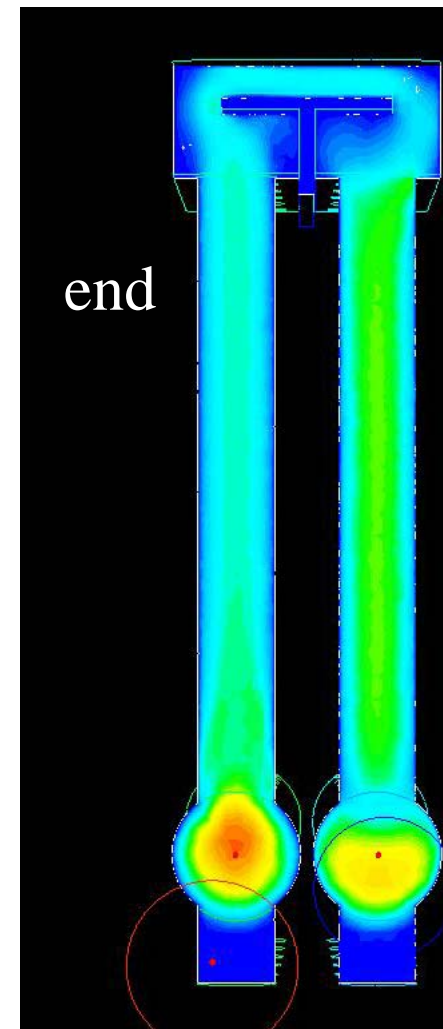
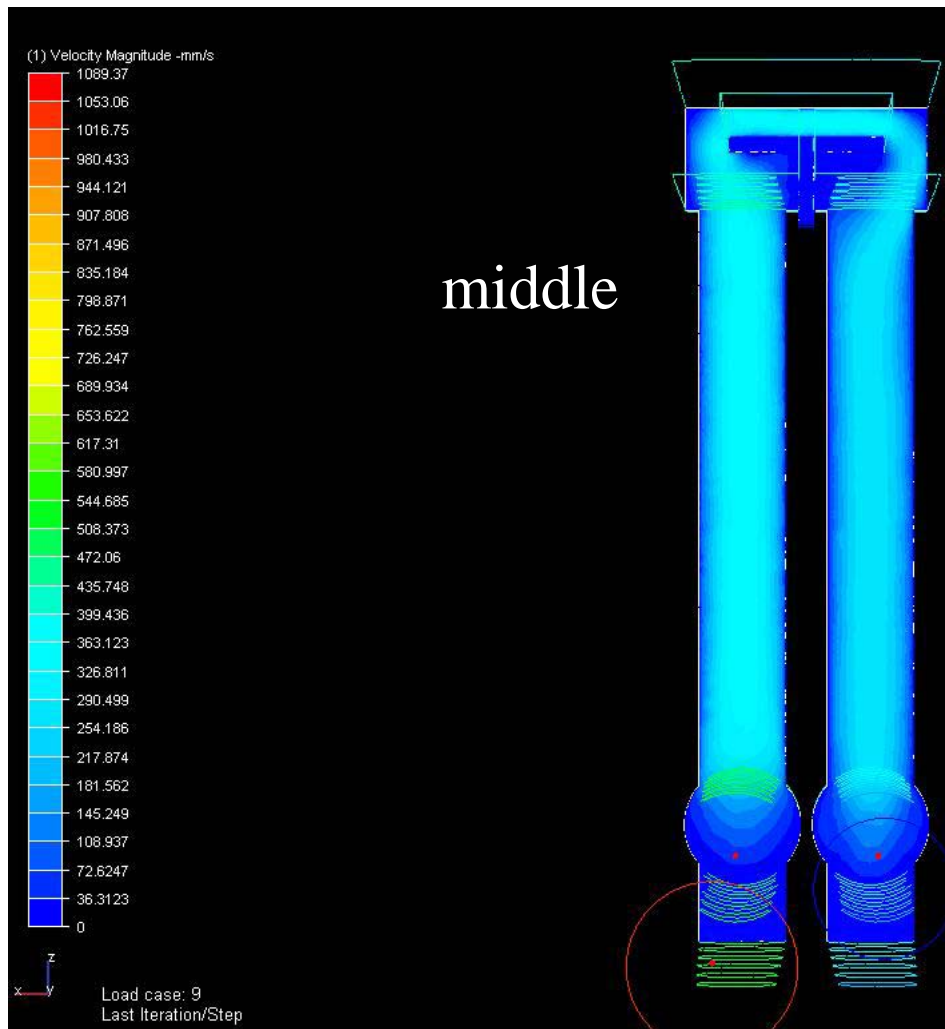
top

vane level

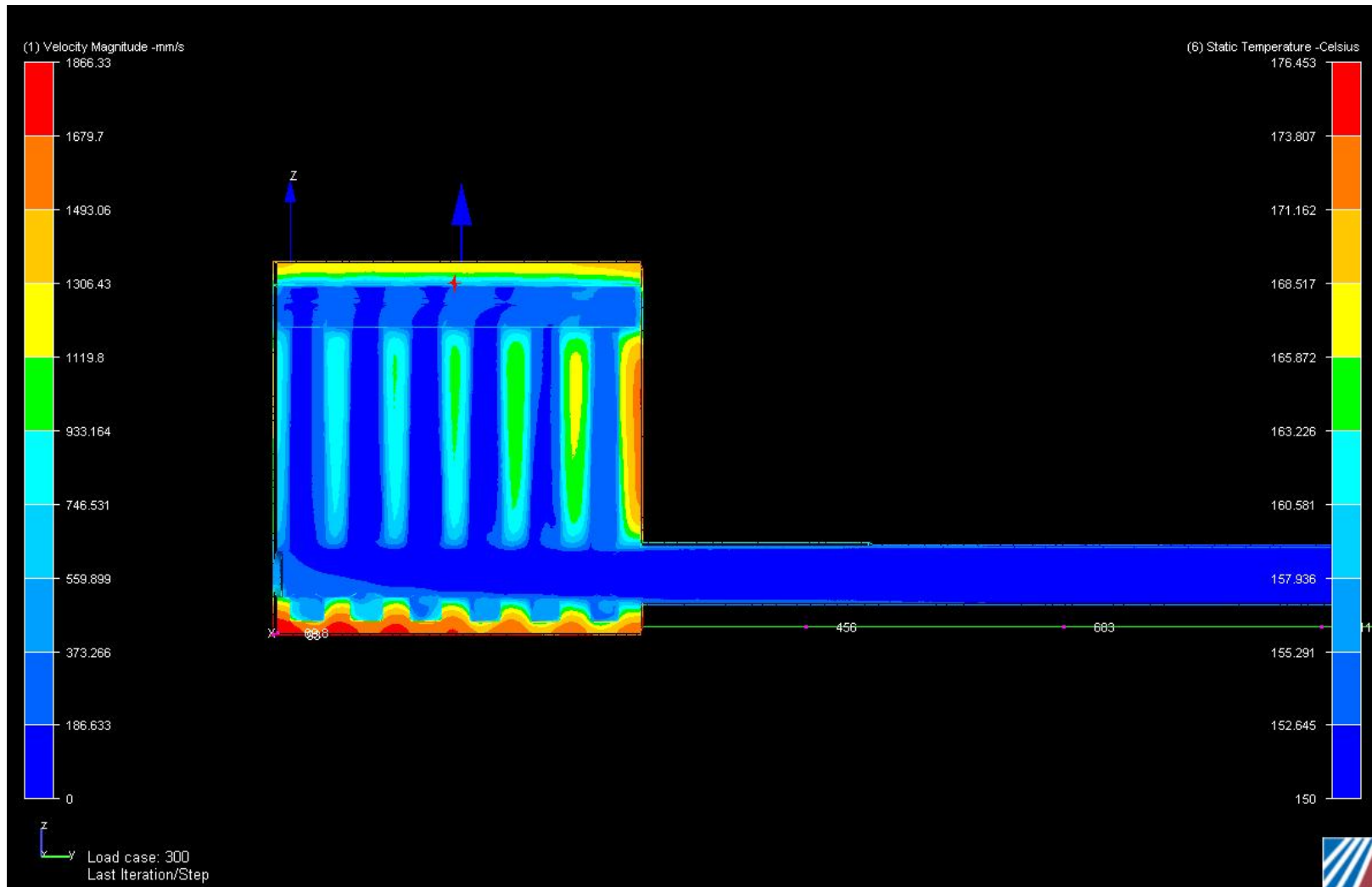
bottom



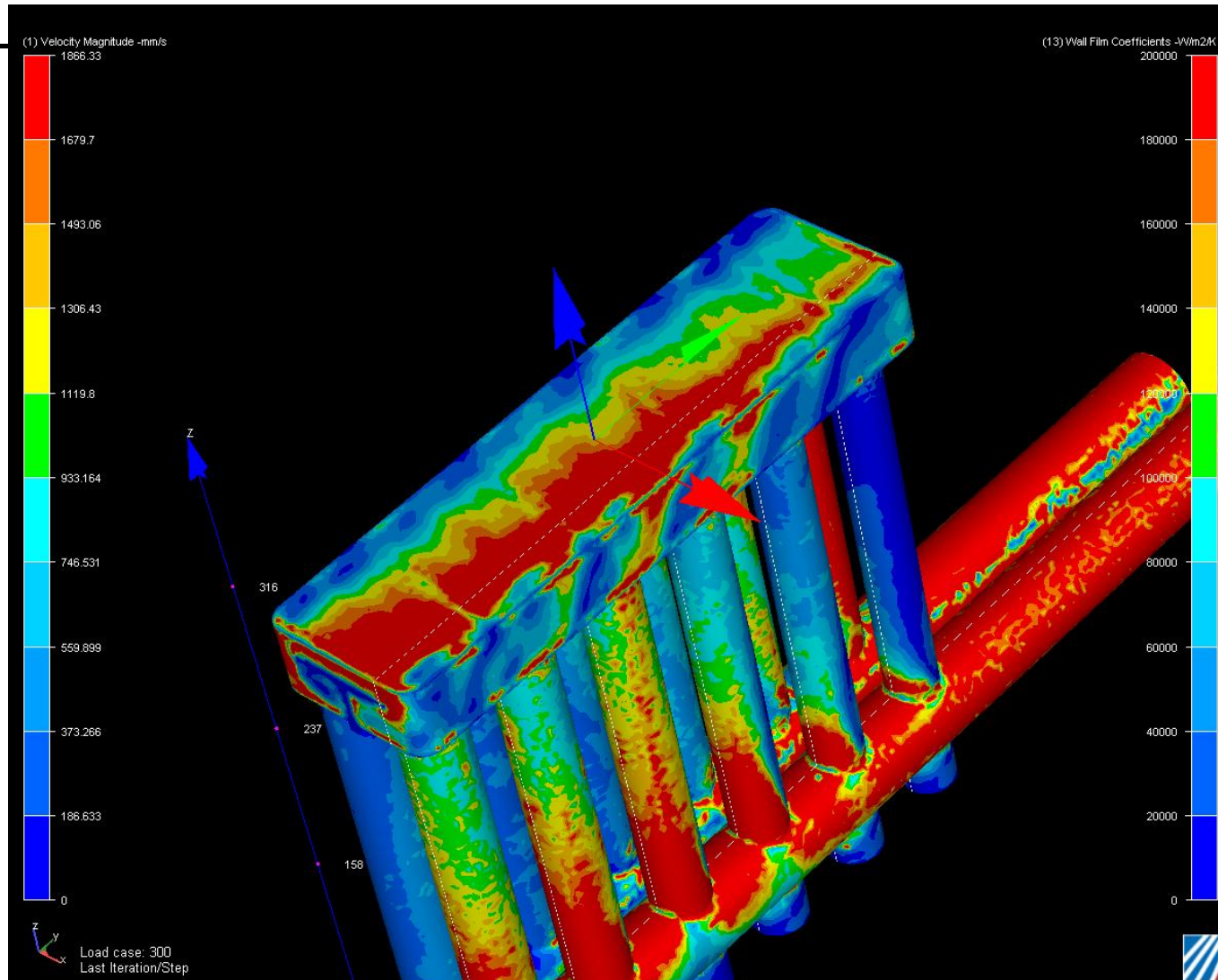
Velocity distributions (con't)



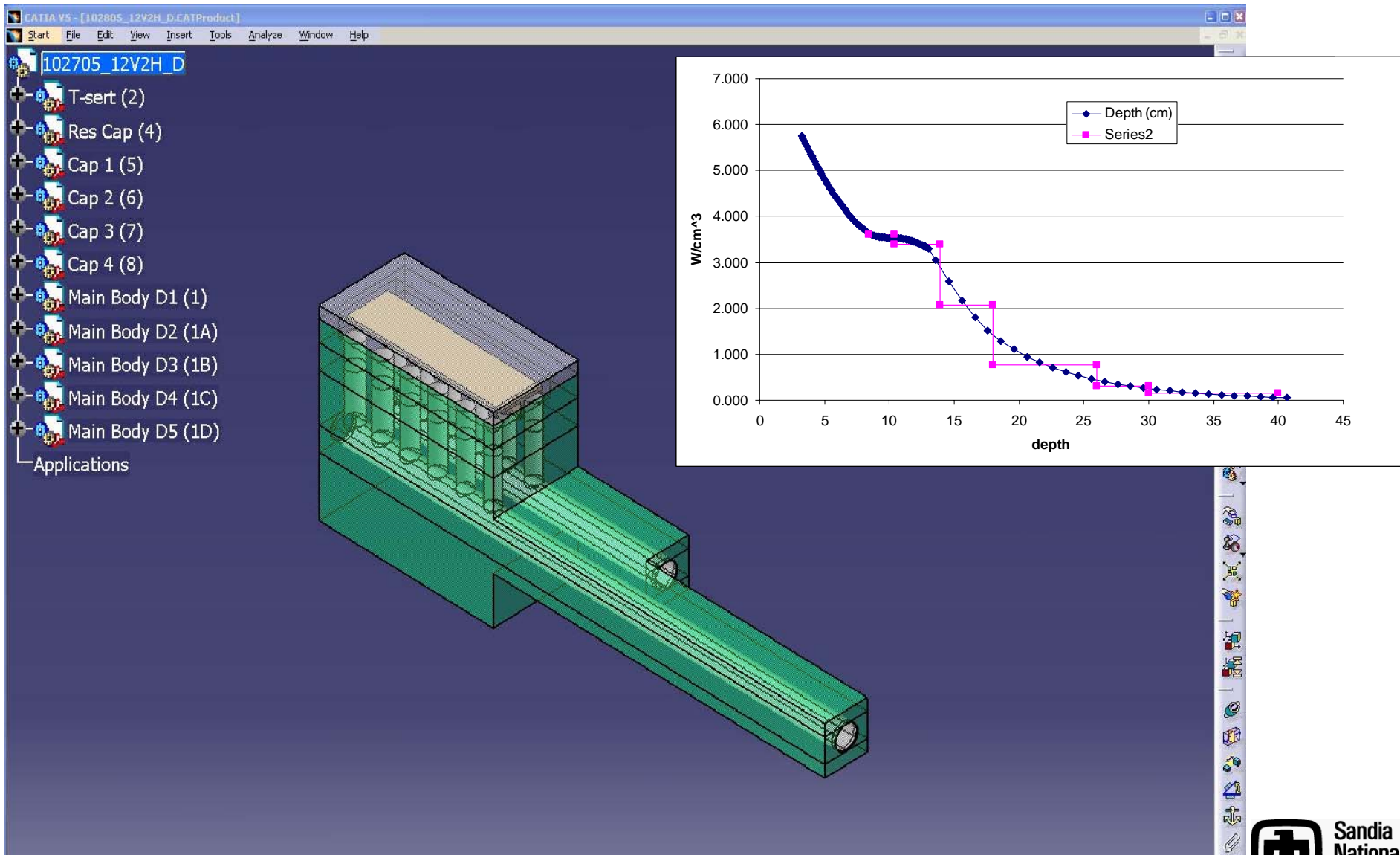
Temperature distribution – uniform $q=3.6 \text{ W/cm}^3$



Wall film coefficient, h



Zoned CFdesign Model





Conclusions

- **US design is evolving**
- **Separate design from manufacturing technique**
- **US favors casting, Int'l team set on forging & machining**
- **Prefer tee divertor vane concept with orificing rather than complicated flow annuli used in IT Module 4**
- **CFD heat transfer with directly coupled ABAQUS thermal stress analysis to be completed by end of 2005.**